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(54) **METHODS AND SYSTEM FOR STARTING AN ENGINE OF A HYBRID VEHICLE**

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**B60K 6/547** (2007.10)  
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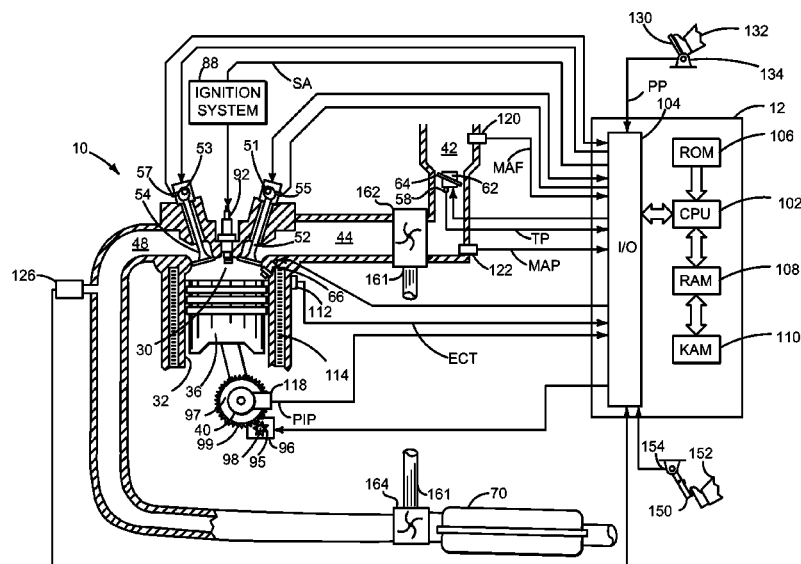
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(57) **ABSTRACT**

Systems and methods for cranking an engine of a hybrid vehicle that includes an electric machine to crank the engine and propel the vehicle are disclosed. In one example, engine cranking speed and engine cranking source are selected in response to vehicle operating conditions that may affect whether or not an electrical power source has sufficient energy to crank the engine.

**13 Claims, 4 Drawing Sheets**



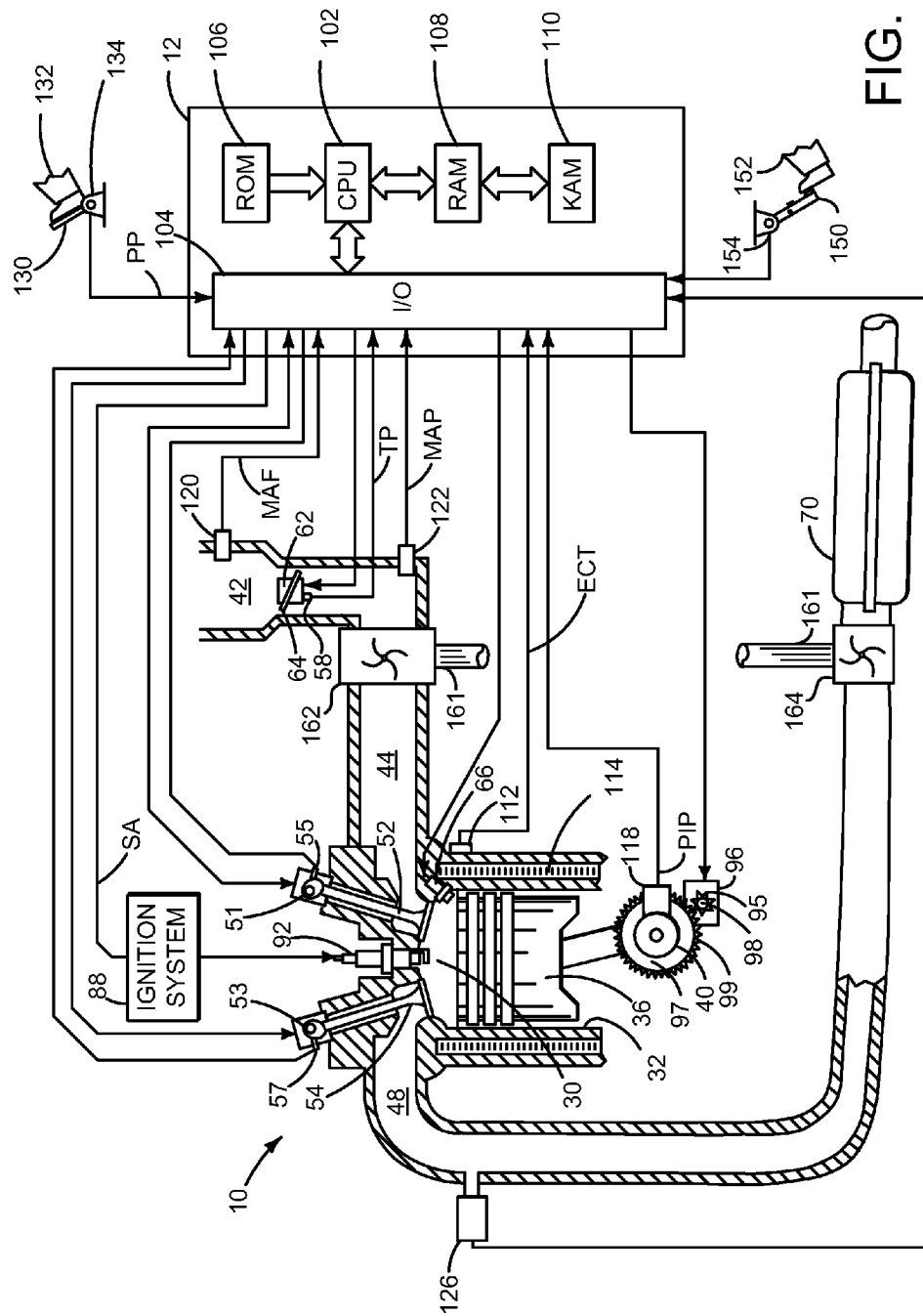


FIG. 1

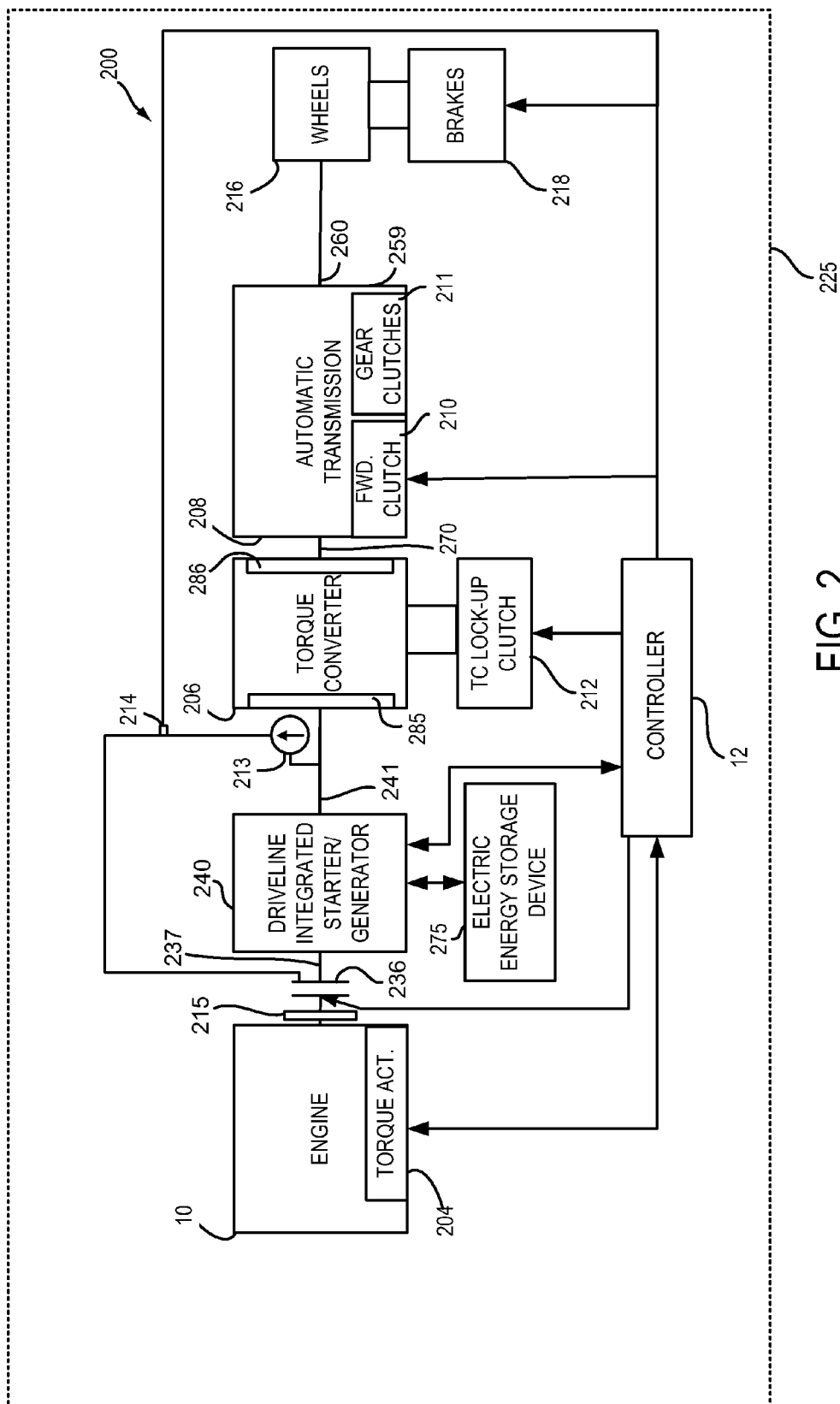


FIG. 2

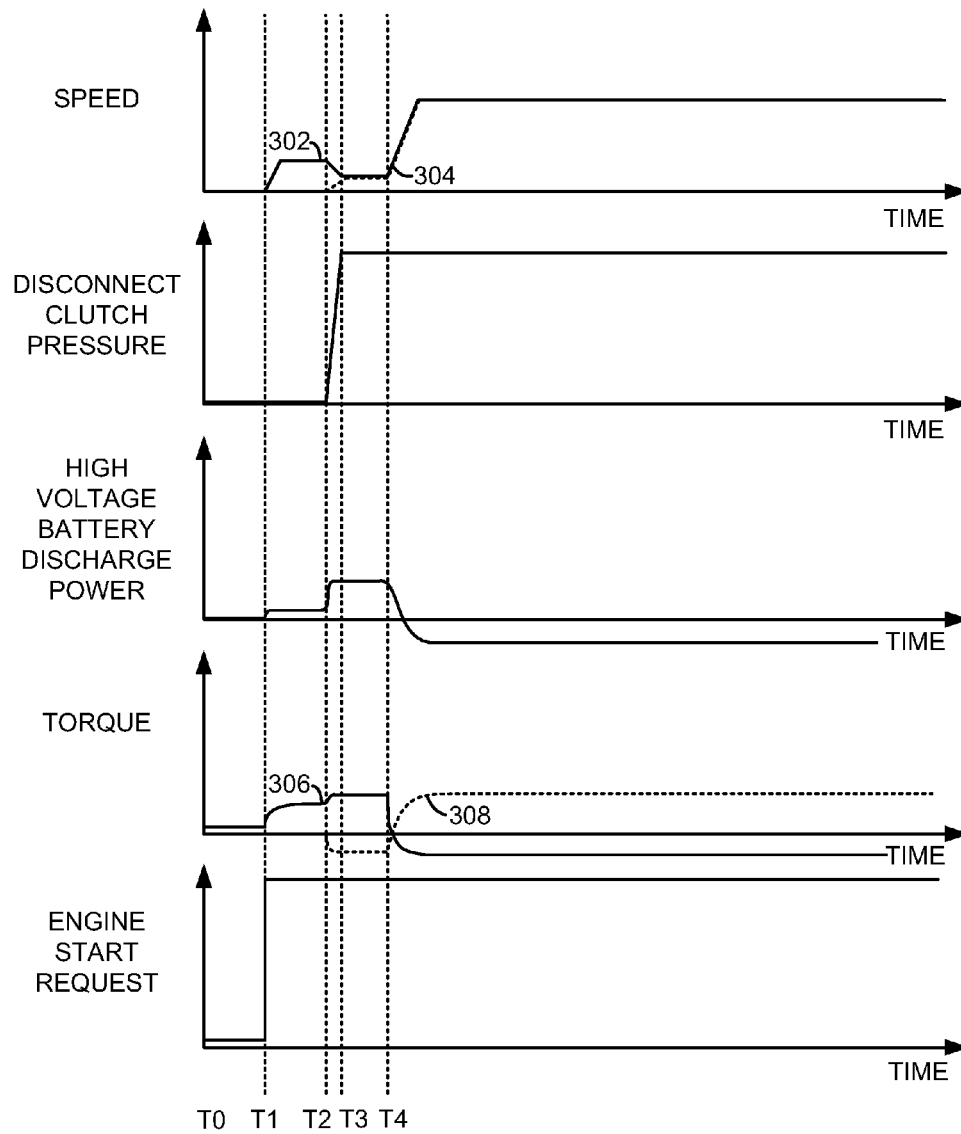


FIG. 3

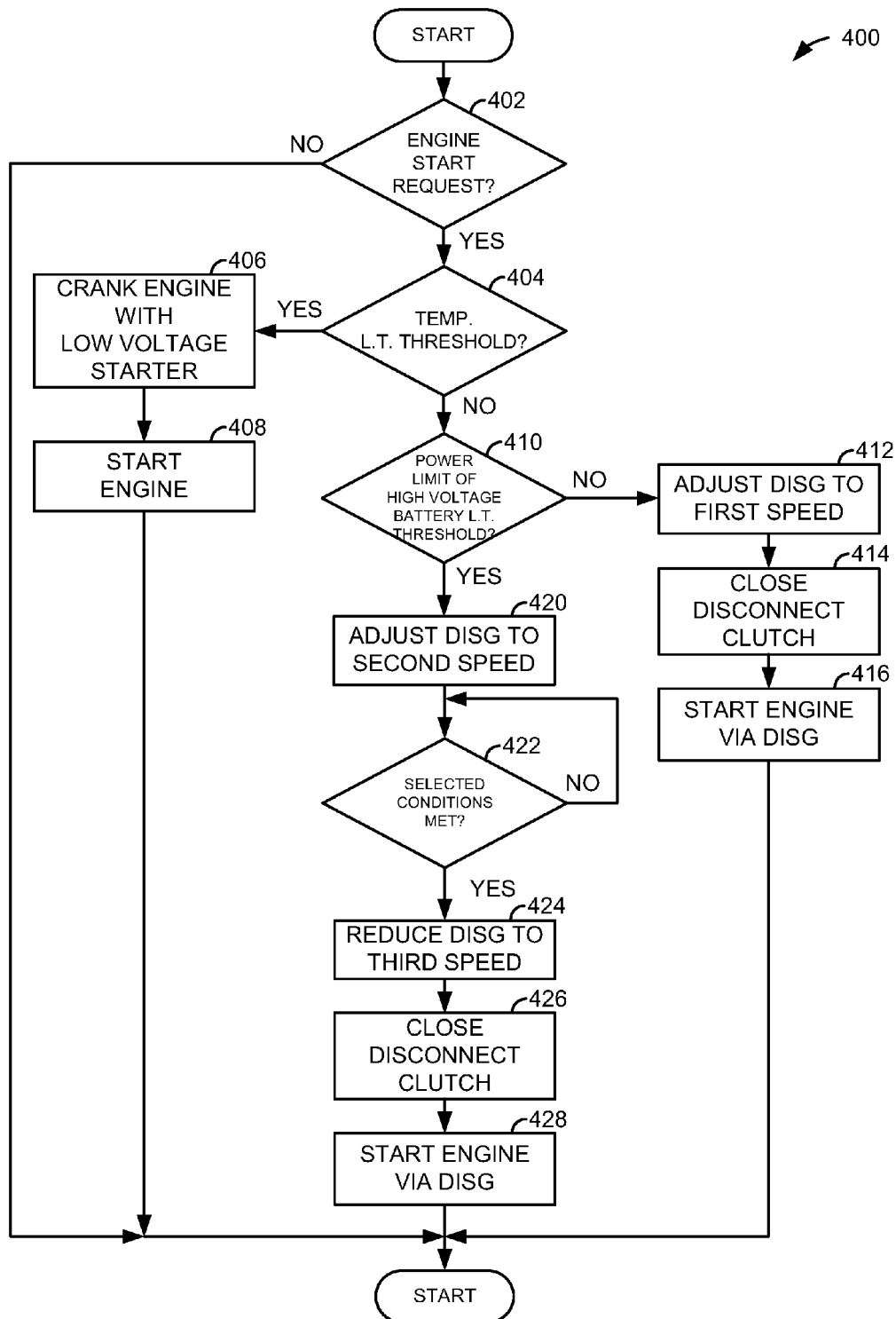


FIG. 4

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## METHODS AND SYSTEM FOR STARTING AN ENGINE OF A HYBRID VEHICLE

### FIELD

The present description relates to methods and a system for starting an engine of a hybrid vehicle during different operating conditions. The methods may be particularly useful for hybrid vehicles that include a driveline disconnect clutch, electric motor, and an engine.

### BACKGROUND AND SUMMARY

An engine of a hybrid vehicle may be started by rotating the engine with a high voltage electric machine and supplying spark and fuel to the engine. The electric machine may rotate the engine to a desired engine idle speed before the engine is supplied with spark and fuel. Alternatively, the electric machine may rotate the engine at a cranking speed (e.g., 200 RPM) at which time spark and fuel may be supplied to the engine. Some hybrid vehicles include a driveline disconnect clutch that is positioned between the engine and the high voltage electric machine. The driveline disconnect clutch allows the high voltage electric machine to operate independently from the engine. Consequently, the vehicle has the capability of being propelled solely via the high voltage electric machine. However, the driveline disconnect clutch may make it more difficult to start the engine at cold ambient temperatures because the driveline disconnect clutch requires a pump to supply it pressurized working fluid in order to close so that the engine may be rotated. Consequently, the high voltage electric machine, engine, and the working fluid pump may have to be rotated by the high voltage electric machine at a time when the battery that provides power to the high voltage electric machine may exhibit reduced output power due at least in part to a lower battery discharge limit.

The inventors herein have recognized the above-mentioned disadvantages and have developed a driveline method, comprising: adjusting an electric machine to a first speed in response to a request to start an engine; adjusting the electric machine to a second speed after achieving the first speed in response to the request to start the engine; and starting an engine via closing a driveline disconnect clutch while or after transitioning the electric machine to the second speed in response to the request to start the engine.

By rotating a driveline at a first speed before lowering driveline speed and cranking an engine at a second speed, it may be possible to provide the technical result of starting the engine at lower temperatures where a battery supplying electrical power to the electric machine may have reduced discharge power limits (e.g., kW). For example, an electric machine may be rotated at a first higher speed to provide working fluid pressure capable of closing a driveline disconnect clutch. After the desired working fluid pressure is achieved, the electric machine speed may be reduced to a speed where the engine may be cranked with less torque than if the engine were cranked at higher speeds. Consequently, a desired working fluid pressure to close a driveline disconnect clutch may be achieved, and the engine may be cranked without the reduced energy storage device discharge limits being exceeded.

The present description may provide several advantages. In particular, the approach may allow an engine to be started during conditions of lower energy storage device discharge limits. Further, the approach may provide alternative ways to

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start an engine of a hybrid vehicle. Further still, the approach may reduce the possibility of vehicle component degradation.

The above advantages and other advantages, and features of the present description will be readily apparent from the following Detailed Description when taken alone or in connection with the accompanying drawings.

It should be understood that the summary above is provided to introduce in simplified form a selection of concepts that are further described in the detailed description. It is not meant to identify key or essential features of the claimed subject matter, the scope of which is defined uniquely by the claims that follow the detailed description. Furthermore, the claimed subject matter is not limited to implementations that solve any disadvantages noted above or in any part of this disclosure.

### BRIEF DESCRIPTION OF THE DRAWINGS

The advantages described herein will be more fully understood by reading an example of an embodiment, referred to herein as the Detailed Description, when taken alone or with reference to the drawings, where:

FIG. 1 is a schematic diagram of an engine;

FIG. 2 shows an example vehicle driveline configuration;

FIG. 3 shows an example engine starting sequence; and

FIG. 4 shows an example method for starting an engine of a hybrid vehicle.

### DETAILED DESCRIPTION

The present description is related to improving engine starting of a hybrid vehicle. The engine may be an engine as shown in FIG. 1 or a diesel engine. The engine may be included in a driveline of a hybrid vehicle as is shown in FIG. 2. The engine may be started according to the method of FIG. 4 as is shown in the sequence of FIG. 3. The method of FIG. 4 provides different ways of starting an engine in response to vehicle operating conditions.

Referring to FIG. 1, internal combustion engine 10, comprising a plurality of cylinders, one cylinder of which is shown in FIG. 1, is controlled by electronic engine controller 12. Engine 10 includes combustion chamber 30 and cylinder walls 32 with piston 36 positioned therein and connected to crankshaft 40. Flywheel 97 and ring gear 99 are coupled to crankshaft 40. Starter 96 (e.g., low voltage (operated with less than 30 volts) electric machine) includes pinion shaft 98 and pinion gear 95. Pinion shaft 98 may selectively advance pinion gear 95 to engage ring gear 99. Starter 96 may be directly mounted to the front of the engine or the rear of the engine. In some examples, starter 96 may selectively supply torque to crankshaft 40 via a belt or chain. In one example, starter 96 is in a base state when not engaged to the engine crankshaft. Combustion chamber 30 is shown communicating with intake manifold 44 and exhaust manifold 48 via respective intake valve 52 and exhaust valve 54. Each intake and exhaust valve may be operated by an intake cam 51 and an exhaust cam 53. The position of intake cam 51 may be determined by intake cam sensor 55. The position of exhaust cam 53 may be determined by exhaust cam sensor 57.

Fuel injector 66 is shown positioned to inject fuel directly into cylinder 30, which is known to those skilled in the art as direct injection. Alternatively, fuel may be injected to an intake port, which is known to those skilled in the art as port injection. Fuel injector 66 delivers liquid fuel in proportion to the pulse width from controller 12. Fuel is delivered to

fuel injector **66** by a fuel system (not shown) including a fuel tank, fuel pump, and fuel rail (not shown).

In addition, intake manifold **44** is shown communicating with turbocharger compressor **162**. Shaft **161** mechanically couples turbocharger turbine **164** to turbocharger compressor **162**. Optional electronic throttle **62** adjusts a position of throttle plate **64** to control air flow from air intake **42** to compressor **162** and intake manifold **44**. In one example, a high pressure, dual stage, fuel system may be used to generate higher fuel pressures. In some examples, throttle **62** and throttle plate **64** may be positioned between intake valve **52** and intake manifold **44** such that throttle **62** is a port throttle.

Distributorless ignition system **88** provides an ignition spark to combustion chamber **30** via spark plug **92** in response to controller **12**. Universal Exhaust Gas Oxygen (UEGO) sensor **126** is shown coupled to exhaust manifold **48** upstream of catalytic converter **70**. Alternatively, a two-state exhaust gas oxygen sensor may be substituted for UEGO sensor **126**.

Converter **70** can include multiple catalyst bricks, in one example. In another example, multiple emission control devices, each with multiple bricks, can be used. Converter **70** can be a three-way type catalyst in one example.

Controller **12** is shown in FIG. 1 as a conventional microcomputer including: microprocessor unit **102**, input/output ports **104**, read-only memory **106** (e.g., non-transitory memory), random access memory **108**, keep alive memory **110**, and a conventional data bus. Controller **12** is shown receiving various signals from sensors coupled to engine **10**, in addition to those signals previously discussed, including: engine coolant temperature (ECT) from temperature sensor **112** coupled to cooling sleeve **114**; a position sensor **134** coupled to an accelerator pedal **130** for sensing force applied by foot **132**; a position sensor **154** coupled to brake pedal **150** for sensing force applied by foot **152**, a measurement of engine manifold pressure (MAP) from pressure sensor **122** coupled to intake manifold **44**; an engine position sensor from a Hall effect sensor **118** sensing crankshaft **40** position; a measurement of air mass entering the engine from sensor **120**; and a measurement of throttle position from sensor **58**. Barometric pressure may also be sensed (sensor not shown) for processing by controller **12**. In a preferred aspect of the present description, engine position sensor **118** produces a predetermined number of equally spaced pulses every revolution of the crankshaft from which engine speed (RPM) can be determined.

In some examples, the engine may be coupled to an electric motor/battery system in a hybrid vehicle as shown in FIG. 2. Further, in some examples, other engine configurations may be employed, for example a diesel engine.

During operation, each cylinder within engine **10** typically undergoes a four stroke cycle: the cycle includes the intake stroke, compression stroke, expansion stroke, and exhaust stroke. During the intake stroke, generally, the exhaust valve **54** closes and intake valve **52** opens. Air is introduced into combustion chamber **30** via intake manifold **44**, and piston **36** moves to the bottom of the cylinder so as to increase the volume within combustion chamber **30**. The position at which piston **36** is near the bottom of the cylinder and at the end of its stroke (e.g. when combustion chamber **30** is at its largest volume) is typically referred to by those of skill in the art as bottom dead center (BDC). During the compression stroke, intake valve **52** and exhaust valve **54** are closed. Piston **36** moves toward the cylinder head so as to compress the air within combustion chamber **30**. The point at which piston **36** is at the end of its stroke and closest

to the cylinder head (e.g. when combustion chamber **30** is at its smallest volume) is typically referred to by those of skill in the art as top dead center (TDC). In a process hereinafter referred to as injection, fuel is introduced into the combustion chamber. In a process hereinafter referred to as ignition, the injected fuel is ignited by known ignition means such as spark plug **92**, resulting in combustion. During the expansion stroke, the expanding gases push piston **36** back to BDC. Crankshaft **40** converts piston movement into a rotational torque of the rotary shaft. Finally, during the exhaust stroke, the exhaust valve **54** opens to release the combusted air-fuel mixture to exhaust manifold **48** and the piston returns to TDC. Note that the above is shown merely as an example, and that intake and exhaust valve opening and/or closing timings may vary, such as to provide positive or negative valve overlap, late intake valve closing, or various other examples.

FIG. 2 is a block diagram of a vehicle **225** including a driveline **200**. The driveline of FIG. 2 includes engine **10** shown in FIG. 1. Driveline **200** may be powered by engine **10**. Engine **10** may be started with an engine starting system shown in FIG. 1 or via driveline integrated starter/generator (DISG) **240**. DISG **240** (e.g., high voltage (operated with greater than 30 volts) electrical machine) may also be referred to as an electric machine, motor, and/or generator. Further, torque of engine **10** may be adjusted via torque actuator **204**, such as a fuel injector, throttle, etc.

An engine output torque may be transmitted to an input side of driveline disconnect clutch **236** through dual mass flywheel **215**. Disconnect clutch **236** may be electrically or hydraulically actuated. If disconnect clutch **236** is hydraulically actuated, pump **213** supplies working fluid (e.g., oil) to driveline disconnect clutch **236**. Pump **213** may be incorporated into torque converter **206** or transmission **208**, and pump **213** rotates to supply pressurized working fluid to driveline disconnect clutch **236** and clutches **210-211**. Pump **213** is mechanically driven and it rotates to pressurize working fluid when shaft **241** rotates. Pressure at an outlet of pump **213** may be determined via pressure sensor **214**. The downstream side of disconnect clutch **236** is shown mechanically coupled to DISG input shaft **237**.

DISG **240** may be operated to provide torque to driveline **200** or to convert driveline torque into electrical energy to be stored in electric energy storage device **275**. DISG **240** has a higher output torque capacity than starter **96** shown in FIG. 1. Further, DISG **240** directly drives driveline **200** or is directly driven by driveline **200**. There are no belts, gears, or chains to couple DISG **240** to driveline **200**. Rather, DISG **240** rotates at the same rate as driveline **200**. Electrical energy storage device **275** (e.g., high voltage battery or power source) may be a battery, capacitor, or inductor. The downstream side of DISG **240** is mechanically coupled to the impeller **285** of torque converter **206** via shaft **241**. The upstream side of the DISG **240** is mechanically coupled to the disconnect clutch **236**.

Torque converter **206** includes a turbine **286** to output torque to input shaft **270**. Input shaft **270** mechanically couples torque converter **206** to automatic transmission **208**. Torque converter **206** also includes a torque converter bypass lock-up clutch **212** (TCC). Torque is directly transferred from impeller **285** to turbine **286** when TCC is locked. TCC is electrically operated by controller **12**. Alternatively, TCC may be hydraulically locked. In one example, the torque converter may be referred to as a component of the transmission.

When torque converter lock-up clutch **212** is fully disengaged, torque converter **206** transmits engine torque to

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automatic transmission **208** via fluid transfer between the torque converter turbine **286** and torque converter impeller **285**, thereby enabling torque multiplication. In contrast, when torque converter lock-up clutch **212** is fully engaged, the engine output torque is directly transferred via the torque converter clutch to an input shaft (not shown) of transmission **208**. Alternatively, the torque converter lock-up clutch **212** may be partially engaged, thereby enabling the amount of torque directly relayed to the transmission to be adjusted. The controller **12** may be configured to adjust the amount of torque transmitted by torque converter **212** by adjusting the torque converter lock-up clutch in response to various engine operating conditions, or based on a driver-based engine operation request.

Automatic transmission **208** includes gear clutches (e.g., gears 1-6) **211** and forward clutch **210**. The gear clutches **211** and the forward clutch **210** may be selectively engaged to propel a vehicle. Torque output from the automatic transmission **208** may in turn be relayed to wheels **216** to propel the vehicle via output shaft **260**. Specifically, automatic transmission **208** may transfer an input driving torque at the input shaft **270** responsive to a vehicle traveling condition before transmitting an output driving torque to the wheels **216**.

Further, a frictional force may be applied to wheels **216** by engaging wheel brakes **218**. In one example, wheel brakes **218** may be engaged in response to the driver pressing his foot on a brake pedal (not shown). In other examples, controller **12** or a controller linked to controller **12** may apply engage wheel brakes. In the same way, a frictional force may be reduced to wheels **216** by disengaging wheel brakes **218** in response to the driver releasing his foot from a brake pedal. Further, vehicle brakes may apply a frictional force to wheels **216** via controller **12** as part of an automated engine stopping procedure.

Controller **12** may be configured to receive inputs from engine **10**, as shown in more detail in FIG. 1, and accordingly control a torque output of the engine and/or operation of the torque converter, transmission, DISG, clutches, and/or brakes. As one example, an engine torque output may be controlled by adjusting a combination of spark timing, fuel pulse width, fuel pulse timing, and/or air charge, by controlling throttle opening and/or valve timing, valve lift and boost for turbo- or super-charged engines. In the case of a diesel engine, controller **12** may control the engine torque output by controlling a combination of fuel pulse width, fuel pulse timing, and air charge. In all cases, engine control may be performed on a cylinder-by-cylinder basis to control the engine torque output. Controller **12** may also control torque output and electrical energy production from DISG by adjusting current flowing to and from field and/or armature windings of DISG as is known in the art.

When idle-stop conditions are satisfied, controller **12** may initiate engine shutdown by shutting off fuel and spark to the engine. However, the engine may continue to rotate in some examples. Further, to maintain an amount of torsion in the transmission, the controller **12** may ground rotating elements of transmission **208** to a case **259** of the transmission and thereby to the frame of the vehicle. When engine restart conditions are satisfied, and/or a vehicle operator wants to launch the vehicle, controller **12** may reactivate engine **10** by cranking engine **10** and resuming cylinder combustion.

Thus, the system of FIGS. 1 and 2 provides for a driveline system, comprising: an engine; a low voltage electrical machine mechanically coupled to the engine; a high voltage electric machine; a driveline disconnect clutch positioned between the engine and the high voltage electric machine;

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and a controller including executable instructions stored in non-transitory memory for cranking the engine via the high voltage electric machine or the low voltage electric machine in response to a temperature, and further instructions for adjusting a cranking speed of the engine in response to the temperature only when the high voltage electric machine cranks the engine. The driveline system includes where the cranking speed of the engine is an engine speed where spark and fuel are first supplied to the engine after an engine stop. The driveline system includes where the high voltage electric machine cranks the engine at a second speed after achieving a first speed in response to an engine start request when the temperature is less than a threshold temperature, the first speed greater than the second speed. The driveline system includes where the high voltage electric machine cranks the engine without engine speed being reduced after an engine stop when the temperature is greater than the threshold temperature. The driveline system further comprises additional instructions for reducing the cranking speed of the engine in response to battery power limits.

Referring now to FIG. 3, an example engine starting sequence for a hybrid vehicle during cold operating conditions is shown. The sequence of FIG. 3 may be provided by the system of FIGS. 1 and 2 executing the method of FIG. 4.

The first plot from the top of FIG. 3 is a plot of high voltage electric machine speed (DISG) and engine speed versus time. The high voltage electric machine speed and engine speed increase in the direction of the Y axis arrow. High voltage electric machine speed is indicated by the solid trace **302**. Engine speed is represented by dotted line **304**. The X axis represents time and time increases from the left side of FIG. 3 to the right side of FIG. 3.

The second plot from the top of FIG. 3 is a plot of driveline disconnect clutch pressure versus time. Driveline disconnect clutch closing force may be substituted for driveline disconnect clutch pressure. The Y axis represents driveline disconnect clutch pressure and pressure increases in the direction of the Y axis arrow. The driveline disconnect clutch is closed when the disconnect clutch pressure trace is near the Y axis arrow and open when the driveline disconnect pressure trace is near the X axis. The X axis represents time and time increases from the left side of FIG. 3 to the right side of FIG. 3.

The third plot from the top of FIG. 3 is a plot of high voltage energy source (e.g., battery) discharge power versus time. The Y axis represents high voltage energy source discharge power and discharge power increases in the direction of the Y axis arrow. Discharge power is negative below the X axis. The X axis represents time and time increases from the left side of FIG. 3 to the right side of FIG. 3.

The fourth plot from the top of FIG. 3 is a plot of engine torque and high voltage electric machine torque versus time. The Y axis represents torque and torque increases in the direction of the Y axis arrow. High voltage machine torque is represented by solid line **306** and engine torque is represented by dotted line **308**. The X axis represents time and time increases from the left side of FIG. 3 to the right side of FIG. 3.

The fifth plot from the top of FIG. 3 is a plot of an engine start request versus time. The engine start request is asserted when the trace is at a higher level near the Y axis arrow. The engine start request is not asserted when the trace is at a lower level near the X axis. The X axis represents time and time increases from the left side of FIG. 3 to the right side of FIG. 3.



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At time T0, the DISG speed and the engine speed are zero indicating that the vehicle is stopped. The driveline disconnect clutch is in an open state allowing the DISG to rotate independently and/or without rotating engine. The high voltage battery discharge power is also zero indicating that the high voltage battery is not being discharged. The DISG torque and engine torque are also zero. The engine start request is not asserted.

At time T1, the engine start request is asserted in response to a driver or controller request. The engine and DISG temperature are at a low level (not shown) and high voltage battery discharge power may also be low. However, DISG torque and current may be elevated during such conditions when rotating the engine due to increased engine friction, oil viscosity, and battery operating characteristics. The DISG speed is increased to a first speed and the disconnect clutch remains open. Engine speed remains at zero. The DISG rotates pump 213 which supplies pressurized working fluid to the driveline disconnect clutch 236. The high voltage battery discharge power increases as the DISG speed increases and the DISG torque increases. The engine torque remains at zero since the driveline disconnect clutch is open.

At time T2, the DISG speed is decreased to a second speed and the driveline disconnect clutch pressure begins to increase to close the driveline disconnect clutch so that torque may be transferred from the DISG to the stopped engine. The DISG speed may be decreased to the second speed after a predetermined amount of time since the DISG reached the first speed has elapsed. Alternatively, the DISG speed may be decreased to the second speed in response to working fluid pressure at an outlet of pump 213 reaching a threshold pressure. The threshold pressure may be a pressure sufficient to close the driveline disconnect clutch. Reducing the DISG speed to the second speed may reduce the amount of torque the DISG needs to rotate the engine as compared to if the DISG were to rotate the engine at the first speed. Further, the DISG may have additional torque capacity at the second speed as compared to the first speed depending on the first and second speeds and the DISG output torque characteristics. The high voltage battery discharge power increases as DISG torque is increased to maintain DISG speed at the second speed as the driveline disconnect clutch is closed. The engine torque increases in a negative direction as the engine begins to rotate in response to the driveline disconnect clutch closing. The engine start request remains asserted.

At time T3, the driveline disconnect clutch is fully closed and the DISG speed reaches the second speed. The high voltage battery discharge power levels off to a constant value as the engine rotates at the second speed. The DISG torque also levels off at a constant torque that it takes to crank the engine at the second speed and rotate the torque converter impeller. Spark and fuel (not shown) are supplied to the engine so that the engine may be started. The engine start request remains asserted.

At time T4, the engine begins to combust air-fuel mixtures and the engine begins to accelerate the DISG. The DISG torque is reduced and it moves toward a negative torque. The high voltage battery discharge also begins to be reduced as the DISG output torque is reduced in response to the engine accelerating. The driveline disconnect clutch remains locked and engine torque increases in a positive direction. The engine start request remains asserted.

In this way, it may be possible to first rotate the driveline at a speed where a desired working fluid pressure to close the driveline disconnect clutch is provided by a pump that is mechanically driven by the driveline. Further, the driveline

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speed may then be reduced to a speed where engine friction may be reduced and/or DISG output torque may be increased so that the DISG may have sufficient torque to rotate the engine at lower ambient temperatures. Thus, working fluid pressure may be increased and engine friction may be held to a lower value to improve the possibility of engine starting at low ambient temperatures.

Referring now to FIG. 4, a method for starting an engine of a hybrid vehicle is shown. The method of FIG. 4 may provide the operating sequence shown in FIG. 3. Additionally, the method of FIG. 4 may be included in the system of FIGS. 1 and 2 as executable instructions stored in non-transitory memory.

At 402, method 400 judges if there is an engine start request. An engine start request may be originated by a driver or a controller. A driver may initiate an engine start request by turning a key or operating a pushbutton. A controller may initiate an engine start request via changing state of a variable in memory or a state of an output. If method 400 judges that there is an engine start request, the answer is yes and method 400 proceeds to 404. Otherwise, method 400 proceeds to exit.

At 404, method 400 judges if a temperature is less than a threshold temperature. In one example, the temperature is an engine temperature. In another example, the temperature is a DISG temperature. In still another example, the temperature is an energy storage device temperature. In still other examples, method 400 may select a lowest temperature from a group of devices not limited to the DISG, battery, engine, ambient air, and oil as a basis for comparing to the threshold temperature. If method 400 judges that the temperature is less than the threshold temperature, the answer is yes and method 400 proceeds to 404. Otherwise, the answer is no and method 400 proceeds to 412.

At 406, method 400 cranks the engine via a low voltage electrical machine or a starter motor 96. The starter motor is supplied power by a low voltage battery (e.g., less than 30 volts). The low voltage electrical machine may rotate the engine at a speed of less than 300 RPM. The low voltage starter may be supplied electrical power from a source different than the high voltage energy storage device. Therefore, the low voltage starter may be able to generate more torque than the DISG during some operating conditions such as when reduced battery discharge limits are in effect. Method 400 proceeds to 408 after beginning to crank the engine.

At 408, method 400 supplies spark and fuel to start the engine as the engine is cranked (e.g., rotated) by the low voltage starter. The low voltage starter may rotate the engine at a speed that is different from a speed that the DISG rotates the engine during engine starting. Method 400 proceeds to exit after the engine is started.

At 410, method 400 judges whether or not a battery discharge power limit is less than a threshold. The battery discharge power limit may vary with battery temperature, battery state of charge (SOC), and other conditions. If method 400 judges that the high voltage battery discharge power limit is less than a threshold, the answer is yes and method 400 proceeds to 420. Otherwise, the answer is no and method 400 proceeds to 412.

At 412, method 400 adjusts DISG to a first speed. The first speed may be a speed at which pump 213 provides sufficient pressure to close the driveline disconnect clutch (e.g., 300 RPM) in a predetermined amount of time. Method 400 proceeds to 414 after the DISG is adjusted to the first speed.

At 414, method 400 starts to close the driveline disconnect clutch. The driveline disconnect clutch may be closed

by allowing working fluid to reach the driveline disconnect clutch from pump 213. Method 400 proceeds to 416 after the driveline disconnect clutch begins to close.

At 416, method 400 starts the engine via rotating the engine via the DISG and by supplying spark and fuel to the engine. Spark and fuel may be supplied to the engine as soon as engine position is determined. Method 400 proceeds to exit after the engine is started by rotating the engine at a single cranking speed.

At 420, method 400 adjusts DISG speed to a second speed. In one example, the DISG speed may be adjusted to a speed at which pump 213 provides sufficient pressure to close the driveline disconnect clutch (e.g., 300 RPM) in a predetermined amount of time. The second speed may be different than the first speed described at 412. Further, the second speed may be adjusted or calibrated to different levels based on vehicle operating conditions. Method 400 proceeds to 422 after the DISG speed is adjusted to the first speed.

At 422, method 400 judges whether or not select conditions have been met. In one example, the select condition may be that a threshold time from a time the DISG reaches the first speed. In another example, the select condition may be that an outlet pressure of pump 213 has reached a threshold pressure. If method 400 judges that one or more selected conditions have been met, the answer is yes and method 400 proceeds to 424. Otherwise, the answer is no and method 400 returns to 422.

At 424, method 400 reduces the DISG to a third speed. In one example, the third speed is a speed where engine friction is less than a threshold value and where engine speed is greater than a threshold speed. The third speed is also less than the second speed, and the third speed may be calibrated or adjusted to different speeds based on operating conditions. Method 400 proceeds to 426 after DISG speed begins to be adjusted to the third speed.

At 426, method 400 begins to close the driveline disconnect clutch. The driveline disconnect clutch may be closed via supplying a working fluid to the driveline disconnect clutch. Method 400 proceeds to 428 after the driveline disconnect clutch begins to close.

At 428, method 400 starts the engine via the DISG when DISG speed is at the third speed. The engine is started by supplying spark and fuel to the engine. The driveline disconnect clutch transfers torque from the DISG to the engine when the engine is being started. The engine speed may be ramped to idle speed after engine run-up from cranking speed. Method 400 proceeds to exit after the engine is started.

In this way, an engine of a hybrid vehicle may be started via different electric machines in response to vehicle operating conditions. Further, speeds of the electric machine may be varied between two or more substantially constant speeds during the engine starting process. By operating the driveline at different speeds during engine starting, it may be possible to start the engine even when battery discharging limits are reduced.

Thus, the method of FIG. 4 provides for a driveline method, comprising: adjusting an electric machine to a first speed in response to a request to start an engine; adjusting the electric machine to a second speed after achieving the first speed in response to the request to start the engine; and starting an engine via closing a driveline disconnect clutch while or after transitioning the electric machine to the second speed in response to the request to start the engine. The method includes where the engine is at rest when the electric machine is adjusted to the first speed. The method

includes where the electric machine is adjusted to the second speed in further response to an outlet pressure of a pump. The method includes where the electric machine is adjusted to the second speed in further response to a predetermined amount of time since the first speed was achieved.

In some examples, the method includes where the first speed is greater than the second speed. The method also includes where closing the driveline disconnect clutch while transitioning the electric machine to the second speed includes closing the driveline disconnect clutch after the electric machine achieves the second speed. The method further comprises adjusting engine speed to a desired idle speed after the engine is started.

The method of FIG. 4 also provides for a driveline method, comprising: in response to a first engine start request, adjusting a speed of an electric machine to a first speed and closing a driveline disconnect clutch; and in response to a second engine start request, adjusting the speed of the electric machine to a second speed, adjusting the speed of the electric machine to a third speed after achieving the second speed, and closing the driveline disconnect clutch during transitioning from the second speed to the third speed. The method further comprises adjusting the speed of an electric machine to the first speed and closing the driveline disconnect clutch in response to a temperature of a device during the first engine start request.

In some examples, the method further comprises adjusting the speed of the electric machine to the second speed, adjusting the speed of the electric machine to the third speed after achieving the second speed, and closing the driveline disconnect clutch during transitioning from the second speed to the third speed in response to the temperature of the device during the second engine start request. The method also includes where the device is an engine. The method includes where the device is an energy storage device or the electric machine. The method further comprises starting an engine after beginning to close the driveline disconnect clutch in response to the first and second engine start requests. The method includes where the second speed is greater than the third speed. The method includes where the electric machine is a high voltage electrical machine, and further comprising starting the engine via a low voltage electric machine in response to a third engine start request at an ambient temperature that is less than ambient temperature during the first and second engine start requests.

As will be appreciated by one of ordinary skill in the art, the methods described in FIG. 4 may represent one or more of any number of processing strategies such as event-driven, interrupt-driven, multi-tasking, multi-threading, and the like. As such, various steps or functions illustrated may be performed in the sequence illustrated, in parallel, or in some cases omitted. Likewise, the order of processing is not necessarily required to achieve the objects, features, and advantages described herein, but is provided for ease of illustration and description. Although not explicitly illustrated, one of ordinary skill in the art will recognize that one or more of the illustrated steps or functions may be repeatedly performed depending on the particular strategy being used. Further, the described actions, operations, methods, and/or functions may graphically represent code to be programmed into non-transitory memory of the computer readable storage medium in the engine control system.

This concludes the description. The reading of it by those skilled in the art would bring to mind many alterations and modifications without departing from the spirit and the scope of the description. For example, I3, I4, I5, V6, V8,

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V10, and V12 engines operating in natural gas, gasoline, diesel, or alternative fuel configurations could use the present description to advantage.

The invention claimed is:

1. A driveline method, comprising:  
in response to a first engine start request, adjusting a speed of an electric machine to a first speed and closing a driveline disconnect clutch; and  
in response to a second engine start request, adjusting the speed of the electric machine to a second speed, the second speed different than the first speed, adjusting the speed of the electric machine to a third speed after achieving the second speed, the third speed less than the second speed, and closing the driveline disconnect clutch during transitioning from the second speed to the third speed.
2. The method of claim 1, further comprising adjusting the speed of the electric machine to the first speed and closing the driveline disconnect clutch in response to a temperature of a device being greater than a threshold during the first engine start request.
3. The method of claim 1, where the driveline disconnect clutch is closed during transitioning from the second speed to the third speed in response to the temperature of the device being greater than a threshold during the second engine start request.
4. The method of claim 3, where the device is an engine.
5. The method of claim 3, where the device is an energy storage device or the electric machine.

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6. The method of claim 1, further comprising starting an engine after beginning to close the driveline disconnect clutch in response to the first and second engine start requests.

7. The method of claim 6, where the third speed is based on engine friction less than a threshold.

8. The method of claim 1, where the electric machine is a high voltage electrical machine, and further comprising starting an engine via a low voltage electric machine in response to a third engine start request and an ambient temperature that is less than ambient temperature during the first and second engine start requests.

9. The method of claim 1, further comprising adjusting the speed of the electric machine to the second speed in response to the second engine start request and a power limit of a battery being less than a threshold.

10. The method of claim 9, further comprising adjusting the speed of the electric machine to the first speed in response to the first engine start request and the power limit of the battery being greater than the threshold.

11. The method of claim 1, where the first speed is where a transmission pump provides sufficient pressure to close the driveline disconnect clutch.

12. The method of claim 1, further comprising starting an engine via closing the driveline disconnect clutch.

13. The method of claim 1, where the electric machine is adjusted to the third speed in further response to an outlet pressure of a pump.

\* \* \* \* \*

UNITED STATES PATENT AND TRADEMARK OFFICE  
**CERTIFICATE OF CORRECTION**

PATENT NO. : 9,463,790 B2  
APPLICATION NO. : 14/448917  
DATED : October 11, 2016  
INVENTOR(S) : Scott James Thompson et al.


Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

In the Claims

Column 11, Line 22, Claim 3, replace “1” with “2”.

Signed and Sealed this  
Thirty-first Day of January, 2017

A handwritten signature in black ink, reading "Michelle K. Lee". The signature is written in a cursive, flowing style with a long horizontal flourish at the end.

Michelle K. Lee  
*Director of the United States Patent and Trademark Office*